

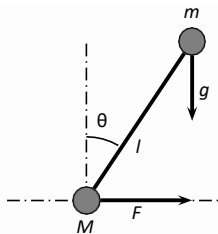
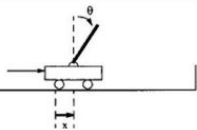
Fuzzy Systems

Fuzzy Control

Prof. Dr. Rudolf Kruse

Fuzzy Controller

Example: Cartpole Problem



Balance an upright standing pole

Lower end of pole can be moved unrestrained along horizontal axis.

Mass m at foot and mass M at head.

Influence of mass of shaft itself is negligible.

Determine force F (control variable) that is necessary to balance pole standing upright.

That is measurement of following output variables:

- angle θ of pole in relation to vertical axis,
- change of angle, *i.e.* triangular velocity $\dot{\theta} = \frac{d\theta}{dt}$

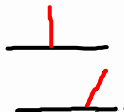
Both should converge to zero.

Qualitative Description of a controller - as Rule System

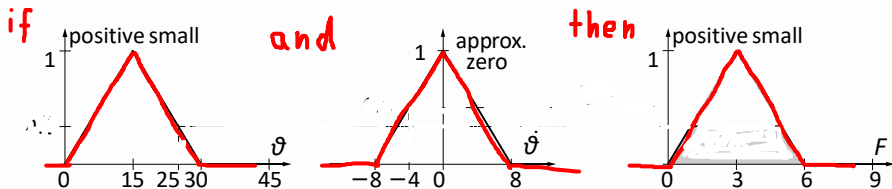
		ϑ						
		nb	nm	ns	az	ps	pm	pb
ϑ	nb			ps	pb			
	nm				pm			
	ns	nm		ns	ps			
	az	nb	nm	ns	az	ps	pm	pb
	ps				ns	ps		pm
	pm				nm			
	pb				nb	ns		

19 rules for cartpole problem, e.g.

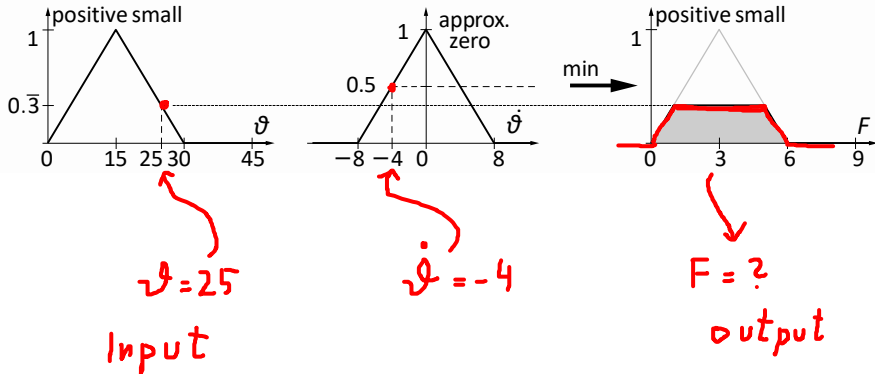
If ϑ is approximately zero and $\dot{\vartheta}$ is negative medium then F is positive medium.



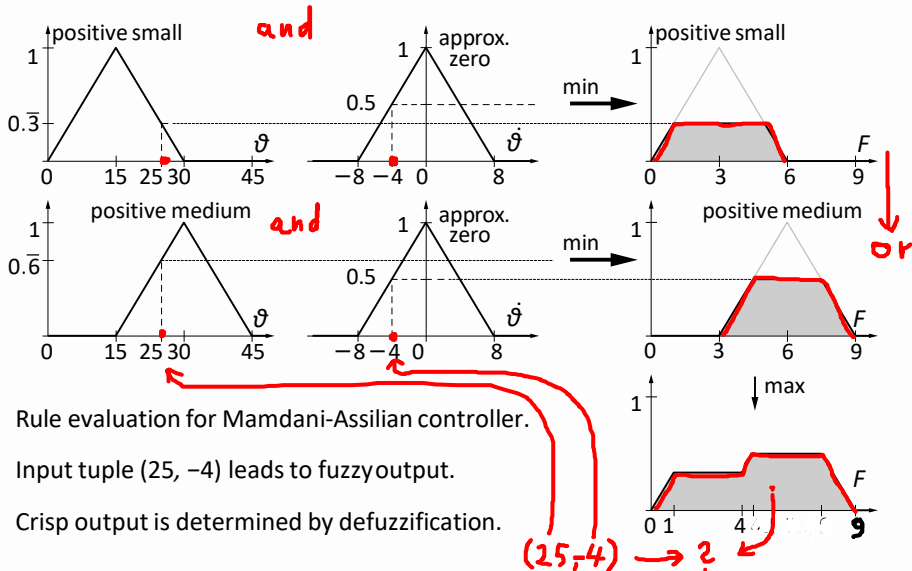
One Rule: Evaluation



One Rule: Evaluation



Several Rules: Evaluation



Rule evaluation for Mamdani-Assilian controller.

Input tuple (25, -4) leads to fuzzy output.

Crisp output is determined by defuzzification.

$(25, -4) \rightarrow ?$

Definition of Table-based Control Function I

Given is the measurement $(x_1, \dots, x_n) \in X_1 \times \dots \times X_n$

Consider a rule R

if $\mu^{(1)}$ and \dots and $\mu^{(n)}$ then η .

The fuzzyfication unit computes for the input (x_1, \dots, x_n) a „degree of fulfillment“ of the premise of the rule:

For $1 \leq v \leq n$, the membership degree $\mu^{(v)}(x_v)$ is calculated. The n degrees are combined conjunctively with the min-operator and give the fulfillment degree α

For each rule R_r with $1 \leq r \leq k$, compute the fulfillment degree α_r

Definition of Table-based Control Function II

For the input (x_1, \dots, x_n) and a rule R the decision unit calculates the output

$$\mu_{x_1, \dots, x_n}^{\text{output}(R)} : Y \rightarrow [0, 1],$$
$$y \mapsto \min (\mu^{(1)}(x_1), \dots, \mu^{(n)}(x_n), \eta(y)).$$

Definition of Table-based Control Function III

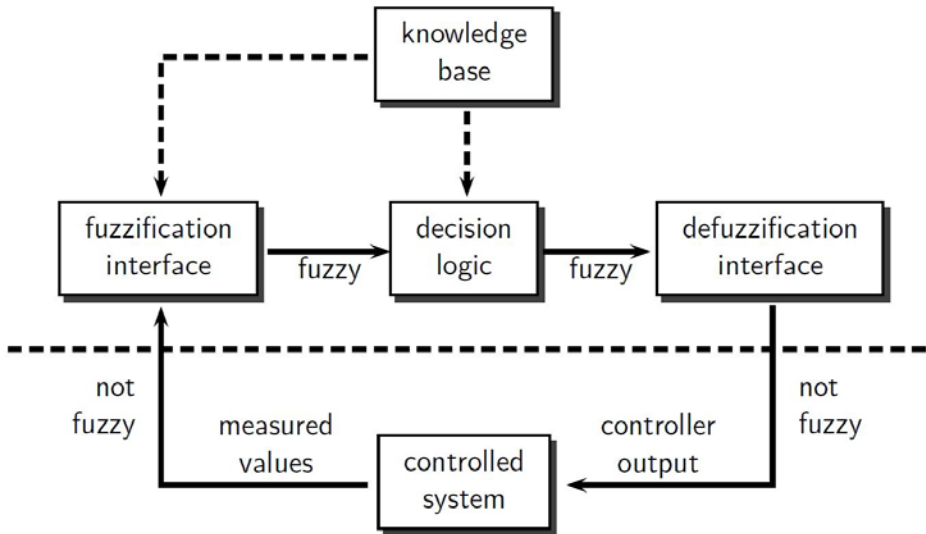
The decision logic combines the output fuzzy sets from all rules R_1, \dots, R_k by using the or-operator **maximum**. This results in the output fuzzy set

$$\mu_{x_1, \dots, x_n}^{\text{output}} : Y \rightarrow [0, 1]$$



Then $\mu_{x_1, \dots, x_n}^{\text{output}}$ is passed to defuzzification interface.

Architecture of a Fuzzy Controller

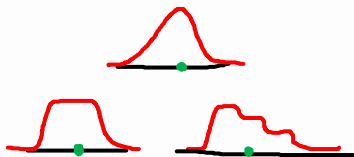


Definition of Table-based Control Function IV

Defuzzification interface derives crisp value from $\mu_{x_1, \dots, x_n}^{\text{output}}$.

Most common **defuzzification** methods:

- max criterion,
- mean of maxima,
- center of gravity.



See Google Patents : More than 1000 methods in real applications

Center of Gravity (COG) Method

η = center of gravity/area of $\mu_{x_1, \dots, x_n}^{\text{output}}$

If Y is finite, then

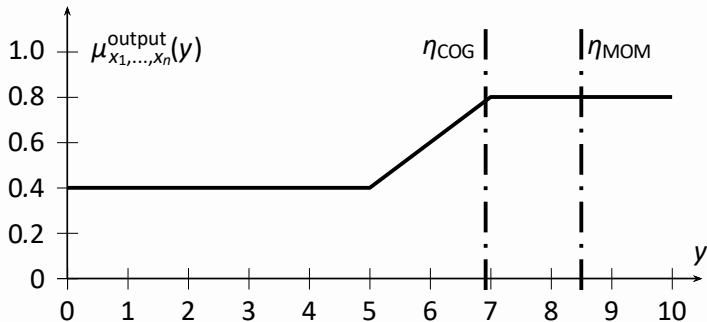
$$\eta = \frac{\sum_{y_i \in Y} y_i \cdot \mu_{x_1, \dots, x_n}^{\text{output}}(y_i)}{\sum_{y_i \in Y} \mu_{x_1, \dots, x_n}^{\text{output}}(y_i)}.$$

If Y is infinite, then

$$\eta = \frac{\int_{y \in Y} y \cdot \mu_{x_1, \dots, x_n}^{\text{output}}(y) dy}{\int_{y \in Y} \mu_{x_1, \dots, x_n}^{\text{output}}(y) dy}.$$

Example

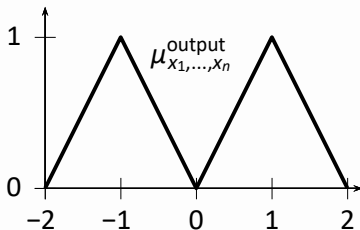
Task: compute η_{COG} and η_{MOM} of fuzzy set shown below.



Example for COG

$$\begin{aligned}\eta_{\text{COG}} &= \frac{\int_0^{10} y \cdot \mu_{x_1, \dots, x_n}^{\text{output}}(y) dy}{\int_0^{10} \mu_{x_1, \dots, x_n}^{\text{output}}(y) dy} \\ &= \frac{\int_0^5 0.4y dy + \int_5^7 (0.2y - 0.6)y dy + \int_7^{10} 0.8y dy}{5 \cdot 0.4 + 2 \cdot \frac{0.8+0.4}{2} + 3 \cdot 0.8} \\ &\approx \frac{38.7333}{5.6} \approx 6.917\end{aligned}$$

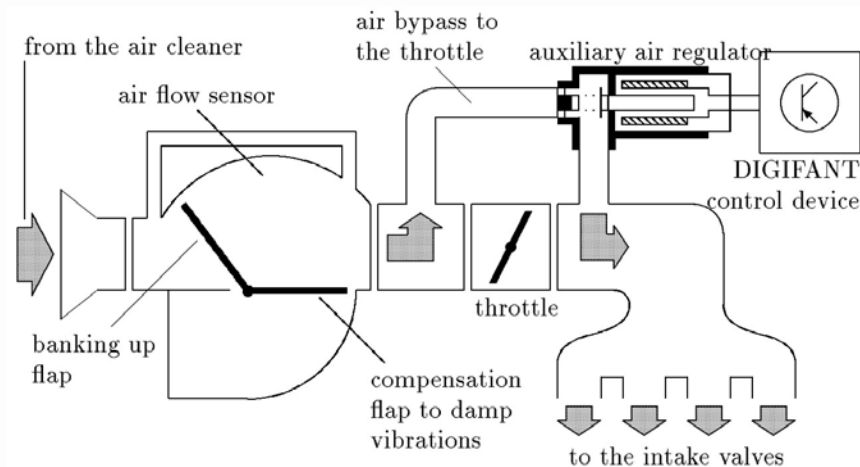
Problem Cases for MOM and COG



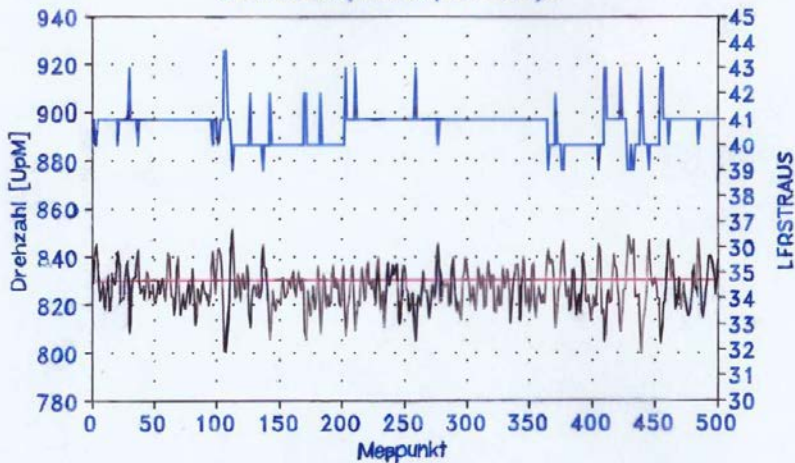
Mamdani Controller

Example: Engine Idle Speed Control

VW 2000cc 116hp Motor (Golf GTI)

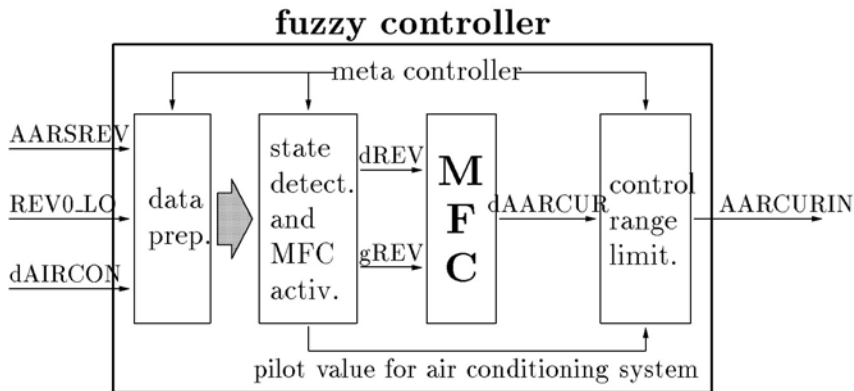


M163B1 Fz SR stat.Zust.
20.8.92 MW(4500MP):827.13UpM



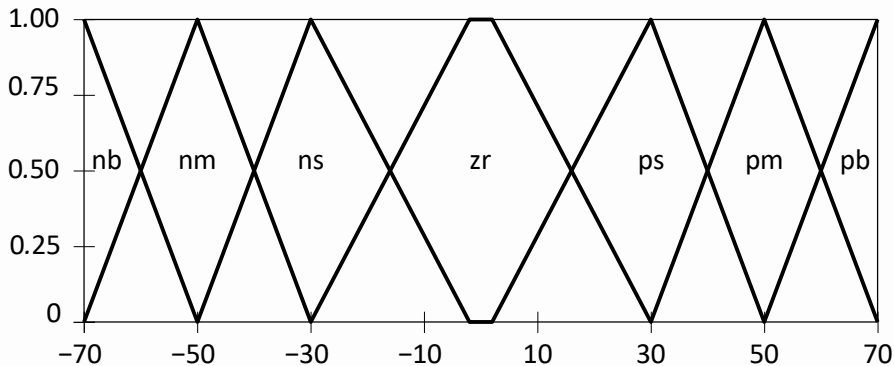
— DRZO_LO — LFRSTRAUS — LFRSDRZ

Structure of the Fuzzy Controller



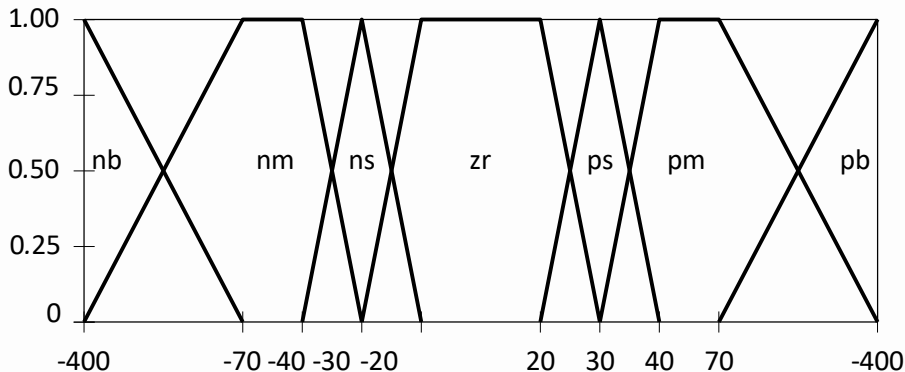
Deviation of the Number of Revolutions

dREV



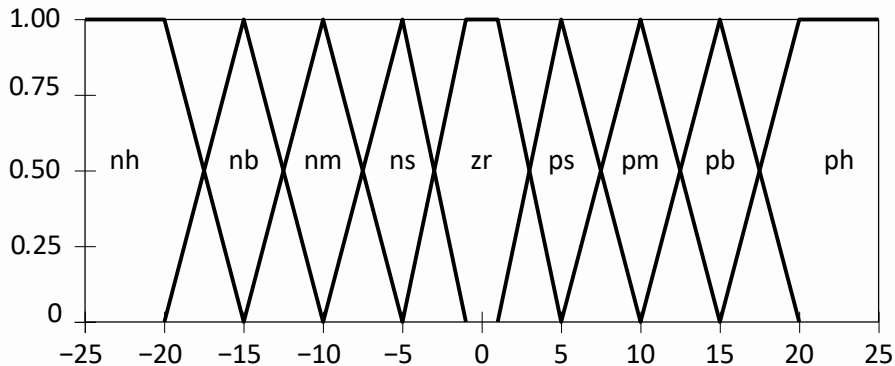
Gradient of the Number of Revolutions

gREV



Change of Current for Auxiliary Air Regulator

dAARCUR



Rule Base

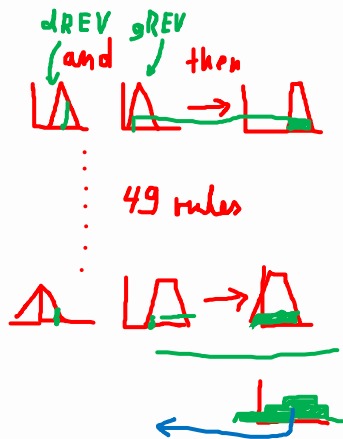
If the deviation from the desired number of revolutions is negative small **and** the gradient is negative medium, **then** the change of the current for the auxiliary air regulation should be positive medium.

		gREV						
		nb	nm	ns	az	ps	pm	pb
dREV	nb	ph	pb	pb	pm	pm	ps	ps
	nm	ph	pb	pm	pm	ps	ps	az
	ns	pb	pm	ps	ps	az	az	az
	az	ps	ps	az	az	az	nm	ns
	ps	az	az	az	ns	ns	nm	nb
	pm	az	ns	ns	ns	nb	nb	nh
	pb	ns	ns	nm	nb	nb	nb	nh

Rule Base

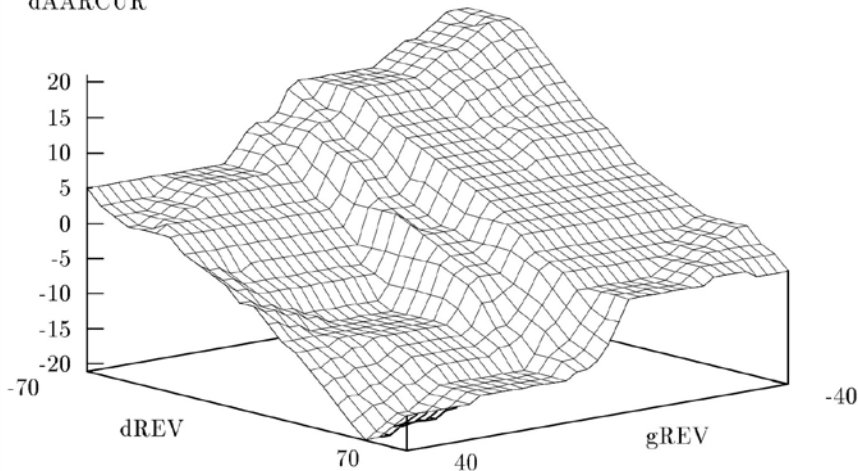
If the deviation from the desired number of revolutions is negative small **and** the gradient is negative medium, **then** the change of the current for the auxiliary air regulation should be positive medium.

		gREV						
		nb	nm	ns	az	ps	pm	pb
dREV	nb	ph	pb	pb	pm	pm	ps	ps
	nm	ph	pb	pm	pm	ps	ps	az
	ns	pb	pm	ps	ps	az	az	az
	az	ps	ps	az	az	az	nm	ns
	ps	az	az	az	ns	ns	nm	nb
	pm	az	ns	ns	ns	nb	nb	nh
	pb	ns	ns	nm	nb	nb	nb	nh

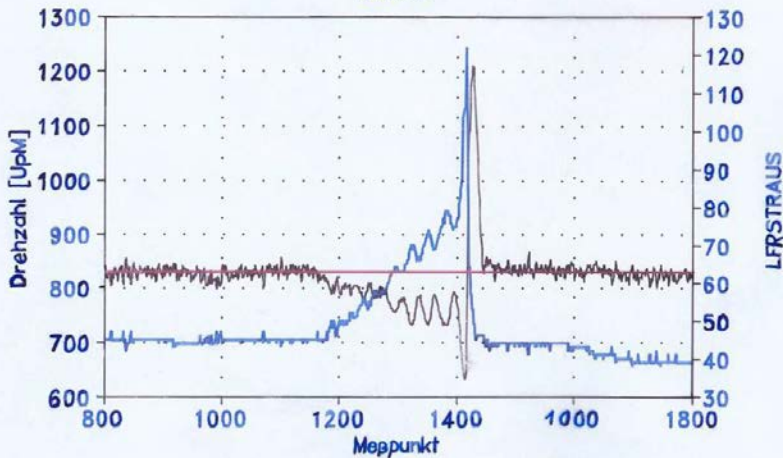


Performance Characteristics

dAARCUR

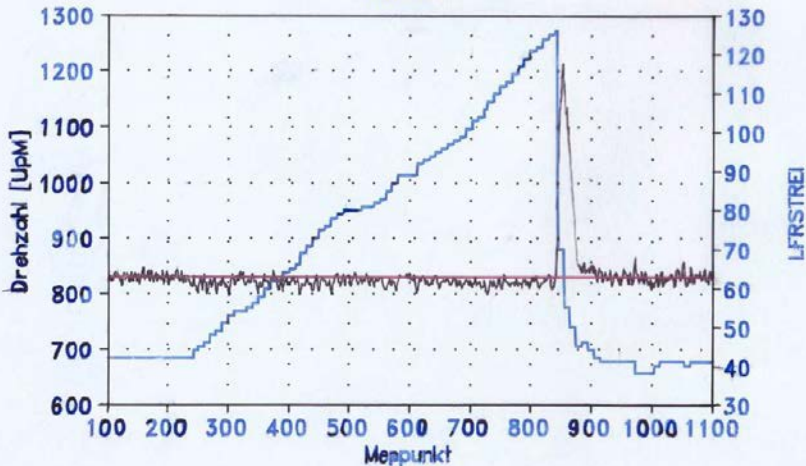


M151B1 Fz SR Kupplung 18.8.92



— DRZO_LO — LFRSTRAUS — LFRSDRE

M155B2 Fz FC Kupplung 18.8.92



— DRZO_LO — LFRSTREI — LFRSDRZ

Example: Automatic Gear Box I

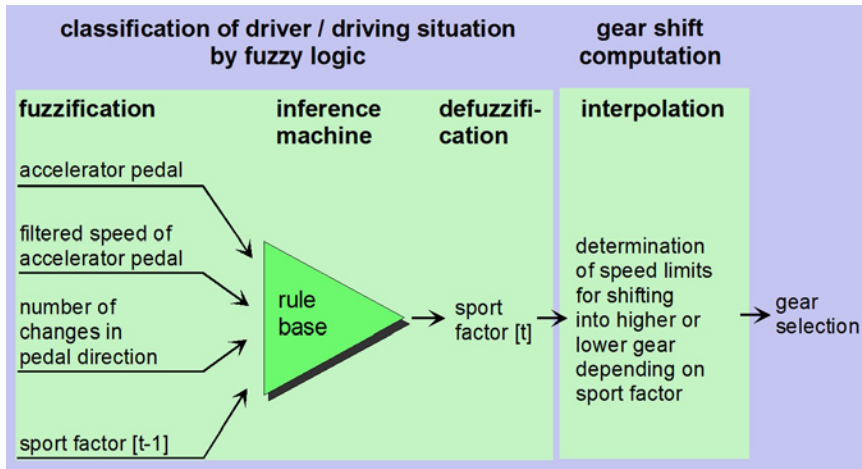
Idea: car “watches” driver and classifies him/her into calm, normal, sportive (assign sport factor $[0, 1]$), or nervous (calm down driver).

Test car: different drivers, classification by expert (passenger).

Simultaneous measurement of 14 attributes, *e.g.* , speed, position of accelerator pedal, speed of accelerator pedal, kick down, steering wheel angle.

Example: Automatic Gear Box II

Continuously Adapting Gear Shift Schedule in VW New Beetle



Example: Automatic Gear Box III

Technical Details

Optimized program on Digimat:

24 byte RAM

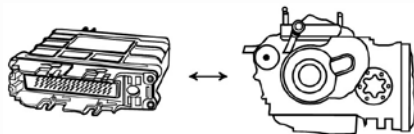
702 byte ROM

uses 7 Mamdani fuzzy rules

Runtime: 80ms

12 times per second new sport

factor is assigned.



Takagi Sugeno Control

Takagi-Sugeno Controller

Proposed by Tomohiro Takagi and Michio Sugeno.

Modification/extension of Mamdani controller.

Both in common: fuzzy partitions of input domain X_1, \dots, X_n .

Difference to Mamdani controller:

- no fuzzy partition of output domain Y ,
- controller rules R_1, \dots, R_k are given by

$$R_r : \text{if } \xi_1 \text{ is } A_{i_1,r}^{(1)} \text{ and } \dots \text{ and } \xi_n \text{ is } A_{i_n,r}^{(n)} \\ \text{then } \eta_r = f_r(\xi_1, \dots, \xi_n),$$

$$f_r : X_1 \times \dots \times X_n \rightarrow Y.$$

- Generally, f_r is linear, i.e. $f_r(x_1, \dots, x_n) = a_0^{(r)} + \sum_{i=1}^n a_i^{(r)} x_i$.

Takagi-Sugeno Controller

For given input (x_1, \dots, x_n) and for each R_r , decision logic computes truth value α_r of each premise, and then $f_r(x_1, \dots, x_n)$.

Analogously to Mamdani controller:

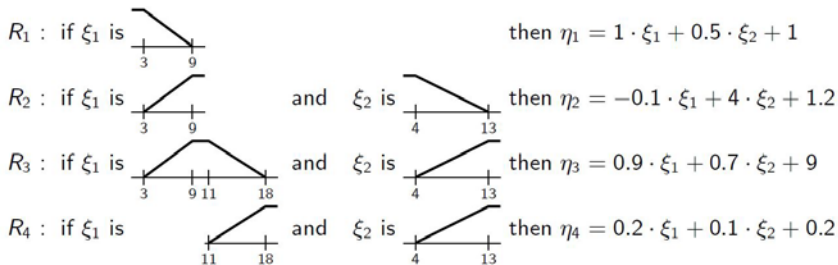
$$\alpha_r = \min \left\{ \mu_{i_1, r}^{(1)}(x_1), \dots, \mu_{i_n, r}^{(n)}(x_n) \right\}.$$

Output equals crisp control value

$$\eta = \frac{\sum_{r=1}^k \alpha_r \cdot f_r(x_1, \dots, x_n)}{\sum_{r=1}^k \alpha_r}.$$

Thus no defuzzification method necessary.

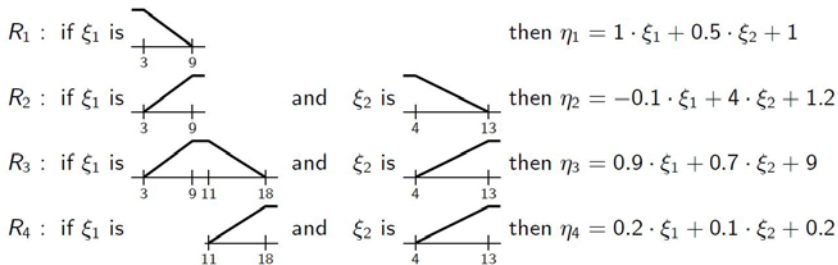
Example



If a certain clause " x_j is $A_{i_j,r}^{(j)}$ " in rule R_r is missing, then $\mu_{i_j,r}(x_j) \equiv 1$ for all linguistic values i_j,r .

For instance, here x_2 in R_1 , so $\mu_{i_2,1}(x_2) \equiv 1$ for all $i_2,1$.

Example



If a certain clause " x_j is $A_{i_j,r}^{(j)}$ " in rule R_r is missing, then $\mu_{i_j,r}(x_j) \equiv 1$ for all linguistic values i_j,r .

For instance, here x_2 in R_1 , so $\mu_{i_2,1}(x_2) \equiv 1$ for all $i_2,1$.

Example: Output Computation

input: $(\xi_1, \xi_2) = (6, 7)$

$$\alpha_1 = 1/2 \wedge 1 = 1/2$$

$$\alpha_2 = 1/2 \wedge 2/3 = 1/2$$

$$\alpha_3 = 1/2 \wedge 1/3 = 1/3$$

$$\alpha_4 = 0 \wedge 1/3 = 0$$

$$\eta_1 = 6 + 7/2 + 1 = 10.5$$

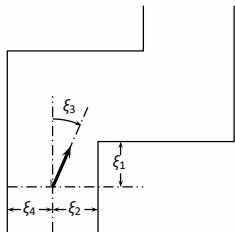
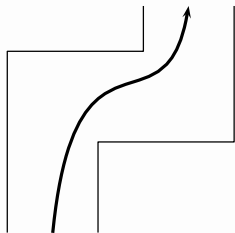
$$\eta_2 = -0.6 + 28 + 1.2 = 28.6$$

$$\eta_3 = 0.9 \cdot 6 + 0.7 \cdot 7 + 9 = 19.3$$

$$\eta_4 = 6 + 7/2 + 1 = 10.5$$

$$\text{output: } \eta = f(6, 7) = \frac{1/2 \cdot 10.5 + 1/2 \cdot 28.6 + 1/3 \cdot 19.3}{1/2 + 1/2 + 1/3} = 19.5$$

Example: Passing a Bend



Pass a bend with a car at constant speed.

Measured inputs:

ξ_1 : distance of car to beginning of bend

ξ_2 : distance of car to inner barrier

ξ_3 : direction (angle) of car

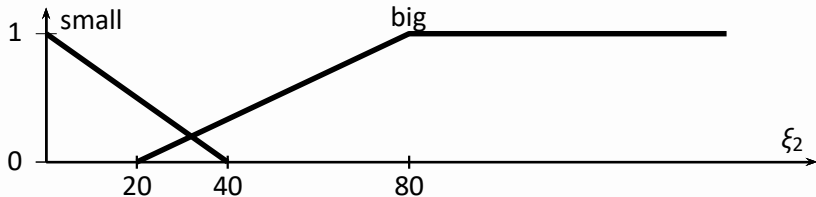
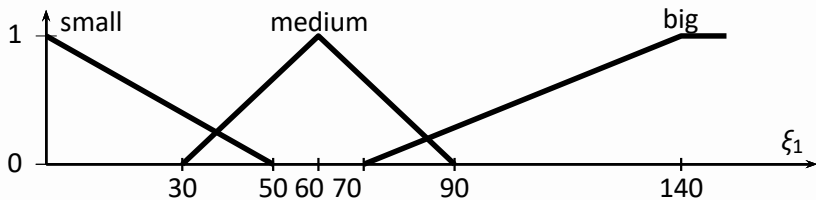
ξ_4 : distance of car to outer barrier

η = rotation speed of steering wheel

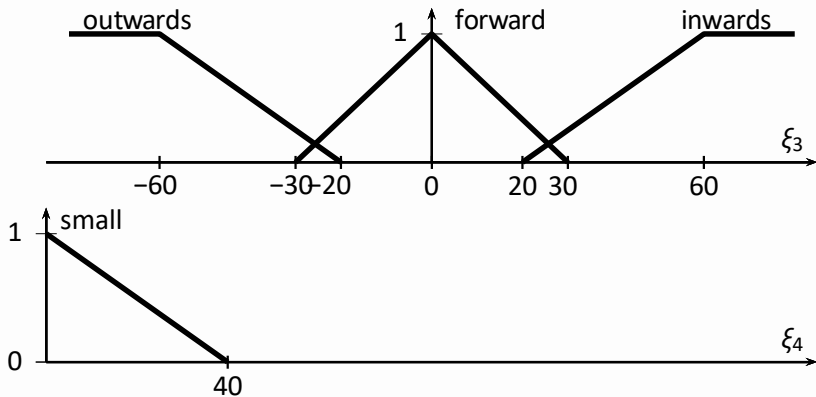
$X_1 = [0\text{cm}, 150\text{cm}]$, $X_2 = [0\text{cm}, 150\text{cm}]$

$X_3 = [-90^\circ, 90^\circ]$, $X_4 = [0\text{cm}, 150\text{cm}]$

Fuzzy Partitions of X_1 and X_2



Fuzzy Partitions of X_3 and X_4



Rules for Car

R_r : if ξ_1 is A and ξ_2 is B and ξ_3 is C and ξ_4 is D

$$\text{then } \eta = p_0^{(A,B,C,D)} + p_1^{(A,B,C,D)} \cdot \xi_1 + p_2^{(A,B,C,D)} \cdot \xi_2 \\ + p_3^{(A,B,C,D)} \cdot \xi_3 + p_4^{(A,B,C,D)} \cdot \xi_4$$

$A \in \{\textit{small}, \textit{medium}, \textit{big}\}$

$B \in \{\textit{small}, \textit{big}\}$

$C \in \{\textit{outwards}, \textit{forward}, \textit{inwards}\}$

$D \in \{\textit{small}\}$

$p_0^{(A,B,C,D)}, \dots, p_4^{(A,B,C,D)} \in \mathbb{R}$

Control Rules for the Car

rule	ξ_1	ξ_2	ξ_3	ξ_4	p_0	p_1	p_2	p_3	p_4
R_1	-	-	outwards	small	3.000	0.000	0.000	-0.045	-0.004
R_2	-	-	forward	small	3.000	0.000	0.000	-0.030	-0.090
R_3	small	small	outwards	-	3.000	-0.041	0.004	0.000	0.000
R_4	small	small	forward	-	0.303	-0.026	0.061	-0.050	0.000
R_5	small	small	inwards	-	0.000	-0.025	0.070	-0.075	0.000
R_6	small	big	outwards	-	3.000	-0.066	0.000	-0.034	0.000
R_7	small	big	forward	-	2.990	-0.017	0.000	-0.021	0.000
R_8	small	big	inwards	-	1.500	0.025	0.000	-0.050	0.000
R_9	medium	small	outwards	-	3.000	-0.017	0.005	-0.036	0.000
R_{10}	medium	small	forward	-	0.053	-0.038	0.080	-0.034	0.000
R_{11}	medium	small	inwards	-	-1.220	-0.016	0.047	-0.018	0.000
R_{12}	medium	big	outwards	-	3.000	-0.027	0.000	-0.044	0.000
R_{13}	medium	big	forward	-	7.000	-0.049	0.000	-0.041	0.000
R_{14}	medium	big	inwards	-	4.000	-0.025	0.000	-0.100	0.000
R_{15}	big	small	outwards	-	0.370	0.000	0.000	-0.007	0.000
R_{16}	big	small	forward	-	-0.900	0.000	0.034	-0.030	0.000
R_{17}	big	small	inwards	-	-1.500	0.000	0.005	-0.100	0.000
R_{18}	big	big	outwards	-	1.000	0.000	0.000	-0.013	0.000
R_{19}	big	big	forward	-	0.000	0.000	0.000	-0.006	0.000
R_{20}	big	big	inwards	-	0.000	0.000	0.000	-0.010	0.000

Sample Calculation

Assume that the car is 10 cm away from beginning of bend ($\xi_1 = 10$).

The distance of the car to the inner barrier be 30 cm ($\xi_2 = 30$).

The distance of the car to the outer barrier be 50 cm ($\xi_4 = 50$).

The direction of the car be "forward" ($\xi_3 = 0$).

Then according to all rules R_1, \dots, R_{20} ,
only premises of R_4 and R_7 have a value $\neq 0$.

Membership Degrees to Control Car

	small	medium	big
$\xi_1 = 10$	0.8	0	0

	small	big
$\xi_2 = 30$	0.25	0.167

	outwards	forward	inwards
$\xi_3 = 0$	0	1	0

	small
$\xi_4 = 50$	0

Sample Calculation (cont.)

For the premise of R_4 and R_7 , $\alpha_4 = 1/4$ and $\alpha_7 = 1/6$,

R_4 yields

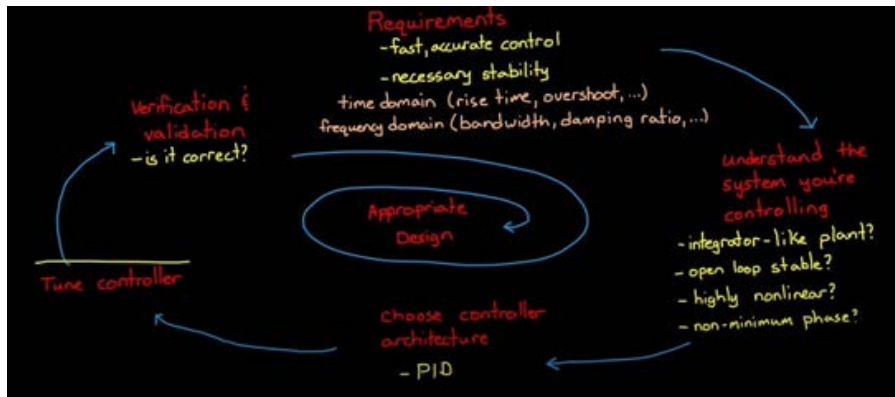
$$\begin{aligned}\eta_4 &= 0.303 - 0.026 \cdot 10 + 0.061 \cdot 30 - 0.050 \cdot 0 + 0.000 \cdot 50 \\ &= 1.873.\end{aligned}$$

R_7 yields

$$\begin{aligned}\eta_7 &= 2.990 - 0.017 \cdot 10 + 0.000 \cdot 30 - 0.021 \cdot 0 + 0.000 \cdot 50 \\ &= 2.820.\end{aligned}$$

The final value for control variable is thus

$$\eta = 2.2518.$$



Control System Design

References

